<u>In the Claims:</u>

Claims **1 to 14** (Canceled).

1   **15.**   (Currently amended) A method for assisting the driver of a
2   vehicle (10) when performing a driving maneuver formed by
3   a parking or shunting maneuver, a reference trajectory (16)
4   corresponding to the driving maneuver being determined,
5   along which the vehicle [[(19)]] (10) is to be moved, and
6   the steering wheel position to be set in each case and
7   controlling the vehicle (10) along the reference trajectory
8   [[(16, 19)]] (16) being indicated to the driver during the
9   driving maneuver, the vehicle longitudinal speed (v) being
10   influenced independently of the driver in the event of a
11   steering angle deviation (d_{LW}) between the actual steering
12   angle (δ_{act}) actually set by the driver and the desired
13   steering angle (δ_{des}) corresponding to the requested steering
14   wheel position, characterized in that the vehicle
15   longitudinal speed is influenced on the basis of the
16   magnitude of the steering angle deviation (d_{LW}) in such a
17   way that [[the]] a greater [[the]] vehicle retardation <u>is</u>
18   carried out, the greater the magnitude of the steering
19   angle deviation (d_{LW}) <u>is</u>.

4834/WFF:he   - 2 -

16. (Previously presented) The method as claimed in claim 15, characterized in that, during the driving maneuver, depending on the current vehicle position ($x_{F,act}/y_{F,act}/\psi_{F,act}$), a steering angle tolerance band (δ_{min} to δ_{max}) which determines the permissible steering angle is determined and the influence on the vehicle longitudinal speed (v) depends on the tolerance margin ($\delta_{des} - \delta_{min}$ or $\delta_{max} - \delta_{des}$) between the desired steering angle (δ_{des}) and the tolerance band limits (δ_{min} or δ_{max}).

17. (Previously presented) The method as claimed in claim 16, characterized in that, in order to determine the steering angle tolerance band, a rotational angle tolerance band is determined, the actual rotational angle ($\psi_{F,act}$) between the vehicle longitudinal axis (71) and a coordinate axis (y) of a stationary coordinate system (22) being enlarged or reduced until it is just still possible to determine a trajectory to the target position (17).

18. (Previously presented) The method as claimed in claim 16, characterized in that the vehicle longitudinal speed (v) is chosen to be lower, the smaller the magnitude of the tolerance margin ($\delta_{des}-\delta_{min}$ or $\delta_{max}-\delta_{des}$).

19. (Previously presented) The method as claimed in claim 15, characterized in that the vehicle longitudinal speed (v) is chosen to be lower, the greater the magnitude of the steering angle deviation (d_{LW}).

4834/WFF:he

– 3 –

1   **20.** (Currently amended) <u>The method</u> ~~Method~~ as claimed in claim
2   15, characterized in that the vehicle longitudinal speed is
3   influenced by means of speed regulation.

1   **21.** (Previously presented) The method as claimed in claim 15,
2   characterized in that the vehicle (10) is retarded down to
3   a standstill and is kept at a standstill as long as, on the
4   basis of the existing steering angle deviation (d_{LW}), the
5   vehicle (10) would assume a vehicle position during onward
6   travel from which the target position (17) can no longer be
7   reached without a shunting interruption to the driving
8   maneuver.

1   **22.** (Previously presented) The method as claimed in claim 21,
2   characterized in that the vehicle (10) is accelerated again
3   independently of the driver if the driver sets a steering
4   wheel position which leads to a permissible steering angle
5   deviation (d_{LW}).

1   **23.** (Previously presented) The method as claimed in claim 15,
2   characterized in that the steering wheel position to be set
3   is indicated by means for acoustic driver information
4   and/or means for optical driver information (13) and/or
5   means for tactile driver information (40 and 41).

4834/WFF:he   — 4 —

1   **24.** (Currently amended) The method as claimed in claim 23,

2   characterized [[is]] in that the means for tactile driver

3   information (40 and 41) have means for changing the

4   steering wheel torque to be applied by the driver.

1   **25.** (Previously presented) The method as claimed in claim 15,

2   characterized in that the driving maneuver is a parking

3   maneuver and the reference trajectory (16) indicates the

4   ideal route from the actual vehicle position

5   $(x_{F,act}/y_{F,act}/\psi_{F,act})$ into the parking position (17).

1   **26.** (Currently amended) The method as claimed in claim 15,

2   characterized in that, in the case of a vehicle (10) in

3   trailer operation, each vehicle position along the actual

4   reference trajectory [[(19)]] (16) is assigned a desired

5   trailer angle (β_{des}) between the vehicle longitudinal axis

6   (71) and the trailer longitudinal axis (72), and in that

7   the actual trailer angle (β_{act}) is determined and compared

8   with the corresponding desired trailer angle (β_{des}), the

9   vehicle longitudinal speed (v) being influenced

10   independently of the driver in the event of an angular

11   deviation between desired trailer angle (β_{des}) and actual

12   trailer angle (β_{act}).

1   **27.** (Currently amended) A device for implementing a method for

2   assisting [[the]] a driver of a vehicle when performing a

3   driving maneuver formed by a parking or shunting maneuver,

4   maneuver as claimed in claim 15, having means (12) for

4834/WFF:he   - 5 -

5   determining a reference trajectory (16) <u>along which the</u>

6   <u>vehicle (10) is to be moved</u> corresponding to the driving

7   maneuver, [[and]] means (13; 40 and 41) for indicating the

8   steering wheel position to be ·set by the driver and

9   controlling the vehicle (10) along the reference trajectory

10   [[(19),]] <u>(16), an evaluation device, and retardation means</u>

11   <u>(50) and/or forward drive means (51) for influencing</u> the

12   vehicle longitudinal speed (v)<u>, wherein the</u> ~~being~~

13   ~~influenced by~~ retardation means (50) and/or forward drive

14   means (51) [[that]] can be activated independently of the

15   driver if a steering angle deviation (d_{LW}) between the

16   actual steering angle (δ_{act}) actually set by the driver and

17   the desired steering angle (δ_{des}) corresponding ·to the

18   requested steering wheel position is established in [[an]]

19   <u>the</u> evaluation device (12), characterized in that the

20   vehicle longitudinal speed is influenced on the basis of

21   the magnitude of the steering angle deviation (d_{LW}) in such

22   a way that [[the]] <u>a</u> greater [[the]] vehicle retardation <u>is</u>

23   carried out, the greater the magnitude of the steering

24   angle deviation (d_{LW}) <u>is</u>.

1 **28.** (Currently amended) The device as claimed in claim 27,

2   characterized in that means (12) are provided for

3   determining the desired trailer angle (β_{des}) between the

4   vehicle longitudinal axis (71) and <u>a</u> [[the]] trailer

5   longitudinal axis (70)<u> of a trailer being towed by the</u>

6   <u>vehicle</u>, and means for determining the actual trailer angle

7   (β_{act}), in that the evaluation device (12) compares the

4834/WFF:he   - 6 -

8   desired trailer angle (β_{des}) and the actual trailer angle

9   (β_{act}), and in that the retardation means (50) and/or forward

10   drive means (51) of the vehicle (10) are activated in the

11   event of an angular deviation being established between the

12   desired trailer angle (β_{des}) and the actual trailer

13   angle (β_{act}).

[RESPONSE CONTINUES ON NEXT PAGE]

4834/WFF:he   − 7 −